VILLAGE OF WOODVILLE GROUND WATER SURVEY

Ministry
of the
Environment

Ontario

The Honourable
George A. Kerr, Q.C.,
Minister

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Deputy Minister

MINISTRY OF THE ENVIRONMENT

VILLAGE OF WOODVILLE

GROUND WATER SURVEY

D.J. ANDRIJIW

1977

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INTRODUCTION

At the request of the Village of Woodville through the Ministry's Central Region Office, a ground water survey was undertaken to determine the potential of the existing well water supply and if necessary, to locate potential sites within an economic distance from the Village for additional municipal well-water supplies to meet future demands.

The evaluation of the potential of the aquifer was based on data derived from the previous test drilling program and the pumping and water level data from the existing wells. The study to determine other potential water supply areas was based on field examinations and available hydrogeologic data. The study was confined to an area within a radius of about 2 miles (3,2 km.) of the Village of Woodville. Water well records, togographic maps and geologic reports were utilized. A field reconnaissance was made to observe geologic and topographic features. Water samples were collected from wells in the vicinity to determine the chemical quality of ground water in the area.

The water well records used in the study area are listed in Table 1. The location of each well is shown in Figure 1. The well numbering system used in this report relates to the permanent well coding numbers of the Ministry of the Environment.

PRESENT SUPPLIES - EVALUATION AND POTENTIAL

The present municipal water supply system in Woodville consists of a 30-foot (9, 1m) deep well, TW-6-69, drilled into the bedrock. The overburden at this site was 12 feet (3,7m) thick with the main water-bearing zone being the top of the bedrock. This well was tested and found to be capable of yielding 75 gpm (5,7 l/s) on a perennial basis and is presently equipped to pump this quantity of water.

In determining the potential of the present water supply well and the well field, the daily pumpage figures and water level data for the last three years were reviewed. It became immediately apparent from the data that the operational procedure used at the well was unusual. Up until 1977, the well was not pumped daily but rather intermittently between lapses of up to six days. Thus when the well was pumped for a one-day period, flows exceeding 90,000 gallons per day (gpd) (409,131 l/d) were recorded. A cursory examination of the data would therefore suggest that the maximum daily demand was approaching the maximum daily yield of the well, 108,000 gallons (490,957 l). Most of the daily pumpages tabulated, including the so called maximum-day pumpages, therefore do not represent actual daily consumptions. In 1977 the pump operation becomes more daily as the daily pumpage increases and as the ratio between storage and water use becomes smaller.

One estimate of the average daily consumption was made by dividing the total quantity of water pumped during the month by the number of days in that month. Figure 2 shows the graphed results. The figure also shows the total monthly precipitation and the maximum and minimum monthly water levels recorded in the observation well (TW-5-69). This graph indicates that although the average daily demand has been increasing, the average demand has not exceeded 30,000 gpd (136,377 l/d) as of February, 1977.

Another attempt to determine the average-day and maximum-day consumption was made by averaging the actual daily recorded pumpage over the preceeding days when no pumpage occurred. The calculated daily pumpages along with the reported daily pumpages were grouped according to the number of days. The results for 1975 and 1976 are as follows:

Actual or Calculated Daily Pumpage	Number of Days Pumpage Occurred	
	1975	1976
<20,000 gallons (90,918 l)	219	227
20,000 to 35,000 gallons (90,918 to 159,107 l)	124	88
35,000 to 60,000 gallons (159,107 to 272,759 l)	22	51
60,000 gallons	5	7

These results indicate that 86% of the time or approximately 315 days during 1976, the daily consumption did not exceed 35,000 gpd (159,107 l/d) while the maximum day consumption may have been in the order of 60,000 gpd (272,754 l/d) for 51 days. The maximums calculated daily consumption was 69,000 gallons. This would then leave approximately 48,000 gpd (218,203 l/d) for future use from the existing well.

A second well, TW-5-69, located 362 feet (110,3m) away from the production well, is 38 feet (11,6m) deep and is drilled 20 feet (6,1m) into the bedrock. This well also encountered a water bearing zone within the first few feet of the bedrock surface. The well was tested and found to yield 40 gpm (3,0 l/s) on a perennial basis. This well is at present not equipped for production purposes. The consulting hydrologist calculated that if both of the wells were pumped simultaneously, then TW-6-69 should be pumped at 50 gpm (3,8 l/s) and TW-5-69 at 40 gpm (3,0 l/s) for a combined yield of 90 gpm (6,8 l/s).

Because the water-bearing zone occurs within the first few feet of the bedrock surface, the consulting hydrologist recommended in his report on the test drilling project that the water levels should not be allowed to drop more than 3 feet (0,9m) below the bottom of the casing in each well. These levels are calculated to be 21 feet (6,4m) and 15 feet (4,6m) for TW-5-69 and TW-6-69, respectively.

At the time of the test drilling and testing of these wells (late spring and early summer, 1969) the static water level in TW-5-69 and TW-6-69 was 8.4 feet (2,56m) and 8.1 feet (2,47m) below ground level, respectively. A water level recorder was placed on TW-5-69 in 1972. The water level data (Figure 2) indicate that water levels fluctuate annually and are as much as 6.16 feet (1,9m), with the water level attaining a high of 5.60 feet (1,7m) below ground surface in the spring and a low of 11.76 feet (3,6m) below ground surface (1975 data) in the fall. It is assumed that this water level fluctuation is due to seasonal causes and is also occurring in the production well.

From the pumping tests conducted in TW-5-69 and TW-6-69, the consulting hydrologist calculated the effective transmissivity of the aquifer in the area of the two wells to be in the order of 2.0 to 3.0 x 10^4 gpd/ft. (298 to 447 m^2/day). The aquifer coefficients were used in the present prediction of pumping water levels rather than the drawdown trends as used by the consulting hydrologist in his report. Assuming the more conservative transmissivity of 20,000 gpd/ft. (298 m^2/day) the production well, being pumped at 75 gpm (5,7 l/s) continuously for 1 year, would have a calculated drawdown of about 8 feet (2,4m). If the main production well was to be pumped at 50 gpm (3,8 l/s) and TW-5-69 at 40 gpm (3,0 l/s), after 1 year of continuous pumping the drawdown in each well, including mutual interference is calculated to be 7.46 feet (2,3m) and 11.16 feet (3,4m) respectively.

From the test drilling program, the consulting hydrologist recommended that the water level in TW-6-69 and TW-5-69 should not be lowered below 15 feet (4,6m) and 21 feet (6,4m) below ground level during pumping. The data from the recorder have shown that the water level may lower to as much as 11.76 feet (3.6m) below ground surface. Assuming that the greatest pumping demand will be during the periods when the ground water levels are moderately to extremely low, the water levels in TW-6-69 and TW-5-69 could quite conceivably drop to 19.22 feet (5.9m) and 22.92 feet (7,0) after continuous pumping of 90 gpm (6,8 l/s) after 1 year.

GEOLOGY

Bedrock

The bedrock in the study area consists of Paleozoic sedimentary rocks of Upper Middle Ordovician Age. The Woodville study area is underlain by the Lindsay formation of the Simcoe Group of formations.

[1] Liberty, B.A. 1969: Paleozoic Geology of the Lake Simcoe Area, Ontario; Geol. Surv. Canada, Mem. 355, Dept. of Energy, Mines and Resources, Ottawa.

It is generally grey to greenish grey, fine-grained argillaceous limestone. The Limestone is generally very fossiliferous and includes thin shale partings. Liberty[1] has estimated that the Lindsay formation is approximately 185 feet (56,4m) thick on the east side of Lake Simcoe. Well No. 4712 has penetrated 230 feet (70, lm) of bedrock and may have penetrated the underlying Verulam formation of Middle Ordovician Age. This formation consists of grey limestone with alternating shale and claystone. However, the well record does not distinguish the difference in the lithology of the bedrock. The limestone of the Lindsay formation weathers to a loose rubble on flat surfaces. No bedrock outcrops have been observed in the study area. Regionally, the bedrock surface is inclined to the south west. Bedrock surface elevation data were obtained from the water well records and plotted on a map of the area. It appears that the bedrock surface forms two northeast-southwest trending valleys; one of which is located to the northwest of Woodville while the second valley underlies the southern portion of the town. White Creek appears to flow along the main axis of this valley.

Overburden

The overburden in the study area consists of sediments of glacial, glacio-fluvial and glacio-lacustine deposits. The hummocky terrain is due to the presence of drumlins and eskers in the study area. The eskers are oriented generally in a northeast-southwest direction, as are the drumlins. A small esker complex is located immediately south and east of

Woodville; another esker complex starts southwest of Woodville and continues towards Cannington while a third major esker complex is located to the south and east of Woodville. This esker is oriented in a more east-west direction.

The terrain is generally characterized by a clayey to sandy till which was deposited by the Ontario ice lobe during Wisconsinan glaciation. A small silt and clay lake plain is located to the south and southeast of Woodville. This was deposited during the presence of glacial Lake Algonquin in this area. Recent swamp deposits are also noted to the northeast and southwest of Woodville.

The geologic sequence of the overburden is generally a clay and stone or boulder formation overlying the bedrock. Occasionally, a local sand and gravel formation is found between the bottom of the clay and boulders formation and the top of the bedrock. In the areas of the eskers the bedrock is generally overlain by sand and gravel.

The overburden thickness in the study area ranges from 3 feet (0,9m) to 60 feet (18.3m). The overburden was found to be 20 feet (6,1m) thick or less in 60% of the water well records. The esker complex to the south east of Woodville has the thickest deposits of sand and gravel and may be in the order of 50 feet (15,2m) thick.

HYDROGEOLOGY

General

A rock formation or unconsolidated sediments which can yield usable quantities of water is called an aquifer. The ability of an aquifer to yield water is dependant upon its hydraulic characteristics, its thickness and areal extent, and on the amount of recharge in the form of precipitation which reaches the aquifer.

Bedrock

Water in the bedrock moves primarily through interconnected openings such as fractures, joints and bedding planes. Water in interconnected, intergranular pore spaces contributes to storage in the aquifer rather than well yield. The yield from a bedrock well is generally dependant upon the number, size and interconnection of the openings which the well intercepts. As a well penetrates deeper into the bedrock formation, more solution cavaties and/or fractures are likely to be intersected.

The bedrock wells in the study area penetrate from 2 to 230 feet (o,6 to 70,1 m) into the rock; however, the deepest penetrating well resulted in dry conditions. A well penetrating 158 feet (48,2m) into the bedrock did encounter a domestic supply of water. Of the bedrock water well records studied, 51% of the wells encountered water after 2 to 30 feet (0,6 to 9,1m) of bedrock penetration while another 29% of the wells encountered water with an additional 20 feet (6,1m) of bedrock drilling. Only four wells penetrated more than 100 feet (30,4m) of bedrock, however, two of these wells did not find sufficient quantities of water for domestic demands. From the well data it is seen that 80% of the bedrock wells encounter sufficient water supplies within the first 50 feet (15,2m) of bedrock penetration.

Specific capacity, which is the well yield in gallons per minute per foot of drawdown (litres per second per metre) is a measure of the ability of a well to yield water. The specific capacities of the bedrock well vary from less than 0.01 to 23.3 gpm per foot of drawdown (0,002 to 5,8 l/s/m) with about 68% of the bedrock wells having specific capacities of less than 0.5 gpm per foot of drawdown. The development of solution channels and fractures along bedding planes in the bedrock aquifer is heterogeneous with the result that high and low-capacity wells can be found in close proximity.

Overburden

In the overburden, water is transmitted through intergranular openings in the sediments, and hence, the sorting, shape and grain size of the overburden materials affect its ability to transmit water. Water movement through glacial materials varies greatly. Water movement is slow in both vertical and horizontal directions through fine-grained materials such as clay or poorly sorted materials such as till, due to the low permeability of the materials. These materials tend to form poor aquifers. Coarse-grained materials such as sands and gravels have high permeabilities and can be fair to excellent aquifers.

There are several dug wells located in the study area. These wells generally have sufficient yields for domestic supplies, however, several water well records have indicated that some owners having previously dug wells have had to have deeper wells drilled in order to obtain sufficient quantities of water. There are a few drilled wells in the study area that are completed in the overburden. These overburden wells range in depth from 16 to 52.5 feet (4,9 to 16,0m). The specific capacities of these wells range from 0.3 to 10 gpm per foot of drawdown (0,07 to 2,49 l/s/m). The well with the high specific capacity was completed in the esker located to the southwest of Woodville.

Although the sands and gravels of the asker formations are favourable aquifer materials, they are generally found to have only the bottom few feet saturated. Thus the available saturated thickness is the limiting factor of these deposits for water supply production purposes. However, the eskers are good recharge areas and if the eskers are on or near the bedrock surface, they may serve as a means of storage of groundwater to the bedrock.

WATER QUALITY

Chemical

Eight water samples were collected to assess the chemical quality of the ground water and one sample was taken of White Creek. The sampling was undertaken in Woodville and west and south of Woodville. The results of the analyses are shown in Table 2.

Two of the samples were taken of the town supply at different locations. Both showed very hard water but otherwise, the other parameters except for nitrate concentration, all fall within the Ministry's criteria for public drinking supplies. The nitrate content was found to be 9.7 and 9.9 ppm, extremely close to the Ministry's criterion of 10.0 ppm. This nitrate problem has been investigated and reported in the past. From the present sampling, the problem still appears to be prevalent, as seen in the water sample collected from wells within Woodville. The Lane well, sample location H, although located in the centre of Woodville, showed low nitrate concentrations. This may be due to the fact that no heavy pumpage is imposed on the well and only recently recharged water is being drawn in.

From the samples collected, the total dissolved solids ranged from 266 to 686 ppm. Four well water samples exceeded the Ministry's criterion of 500 ppm for total dissolved solids. The hardness concentration of the water is quite variable from 7 to 532 ppm. The sample with 7 ppm hardness content has been treated by a softener.

The chloride concentration of all the samples falls below the Ministry's criterion of 250 ppm as does the sulphate concentration having the same criterion. Two of the well water samples and that of White Creek exceed the Ministry's criterion of 0.3 ppm for iron content. Although the town supply has an iron content of 0.01 ppm, the operator did indicate that some people on the town supply near the pumphouse reported "flecks" of matter in their water. The operator also indicated that some flecks of matter were observed at the well head. This may be precipitating iron caused by the water level being lowered below the main water bearing zone in the well and, in cascading into the well bore, the oxidation of iron takes place leading to the precipitation of iron.

The area to the west of Woodville appears to have low nitrate concentrations, however, one of the sampled wells had water exceeding the criterion for dissolved solids while another sample well showed an iron content greater than the desired criterion.

Some of the water well records have shown that drilling into the bedrock, particularly deeper into the rock, has yielded water containing high chlorides or sulphurous gas.

FAVOURABLE TEST DRILLING AREAS

The overburden aquifer does not appear to be suitable for the construction of high capacity wells, therefore, it appears that any new production wells will have to be drilled in the bedrock.

On the basis of the available hydrogeologic data, the areas shown in Figure 1 appear to be the most favourable for testing. Two of the areas are located near or on the esker complex. Although it is not anticipated that the sand and gravel of the esker will have sufficient saturated thickness to yield large supplies, they may directly overlie the bedrock and thereby, be hydraulically connected with the bedrock aquifer. As a result, the water from the bedrock may be of more acceptable quality than bedrock water in other areas. The water quality in these areas may be favourable except for possibly iron concentrations. The piezometric surface shows that the high nitrates found in the centre of Woodville may not migrate as readily towards these areas as they do towards the present municipal supply.

The sites have also been located on the flanks or centre of the bedrock valleys. The bedrock surface in these locations may be highly weathered from past erosional forces and thereby, the top several feet of the bedrock may have high permeabilities.

These sites are located sufficiently distant from the present municipal supply, whereby, interference from pumping would be negligible, if any. During the test drilling program, data from the pumping tests indicated that about 0.5 feet (0,15m) of drawdown might be anticipated at a distance of 1,000 feet (305m) from the pumped well.

CONCLUSIONS

Based on the pumping test and pumping data of the production well, the present town supply is capable of yielding 90 gpm (6,8/s) on a continuous basis from the two wells. Monitoring of the water levels should be continued to determine if this yield is in fact the maximum or whether the aquifer conditions can allow for increased pumping.

The present average daily pumpage is in the order of 30,000 gpd (136,377 l/d) with the maximum day pumpage being just over 40,000 gpd (181,836 l/d). As the pump operation appears to be more daily, the pumpages presently reflect the daily consumption.

Based on the available hydrogeologic data, the overburden aquifer does not appear to be capable of yielding sufficient quantities of water for municipal supplies. The bedrock is the only aquifer capable of yielding large quantities of water to individual wells, especially where it is hydraulically connected to partially saturated sands and gravels of esker formations.

From the water well records, it appears that a larger quantity of water is derived from the first 30 feet (9,1m) of bedrock. Drilling deeper to 50 feet (15,2m) may yield favourable supplies, however, it appears that with increased depth the chemical water quality changes and the possibility of encountering poorer quality water in the form of higher chlorides and possibly sulphurous odours and gas increases. Therefore, wells drilled to depths of approximately 50 feet (15,2m) may encounter sufficient quantities of water with favourable quality. It is anticipated that the nitrate concentration in the ground water remote from the Village will not be as high as in the Village of Woodville.

The more favourable sites for drilling are described under the heading of "Favourable Test Drilling Areas" and are shown in Figure 1. It is anticipated that local well interference will be minimal and will be dependant upon the rate of pumping of any new well.

RECOMMENDATIONS

It is recommended that TW-5-69 be put into production at the noted 40 gpm (3,0 l/s) and the present production will cut back to 50 gpm (3,8 l/s) for a combined yield of 90 gpm (6,8 l/s) if the present supply of 75 gpm (5,7 l/s) is insufficient to meet the near future demand.

It is recommended that any further test drilling be carried out in the areas shown in this report.

Extended pumping tests should be carried out on any test wells encountering favourable formation to determine their capacity and changes in chemical water quality with respect to pumping time and the anticipated amount of interference, if any, in nearby wells.

Prepared by: D. J. Andrijiw
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Approved by:
T.J. Yakutckik

DJA/im

Ministry of the Environment
Ontario

Table 1 Summary of Water Well Records

Date DEC. 1976

Prepared by D. J. A.

Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm) (hrs)	Pumping Level (feet)	Quality	Use	Remarks, Log etc
160	MARIPOSA TWP. 874	XIII	1	C. JEWELL	J.F. HENDERSON 1964	⚲	6¼	77	33	¾ 1	77	FR	D S	0 dugwell 25 lmst 77 *45
3868	" 910	XIII	3	J. PARLIAMENT	J.F. HENDERSON 1969	⚲	6¼	49	35	9 2½	35	FR.	D	0 dug 35 lmst. 49 *47
2161	" 881	XIII	7	M. BUDD	J.F. HENDERSON 1964	⚲	6¼	58	20	20 4	45	FR	S	0 tpsl 2 sndy soil 47 lmst 58 *58
2162	" 930	XIII	8	J. SCHWAIZWALD	KING 1957	●	5⅝	48	36	5 ½	46	FR	D	0 grvl & cl 48 *42
2167	" 868	XIV	1	DOBBS	BALDWIN 1965	●	6¼.	33	8	10 1	8	FR.	D	0 dug 15 snd & grvl 33 * 28-32
3933	" 885	XIV	1	E. SMART	J.F. HENDERSON 1969	●	6¼	31	8	9 2	14	FR	D	0 tpsl 2 cl, stns 16 cl, snd, grvl 31 *30
5908	" 895	XIV	2	W. TEEFY	FAULKNER 1974	⚲	6¼	33	10	6 3	28	FR	D	0 predrilled 22 lmst 33 *22
5697	" 895	XIV	2	W. TEEFY	FAULKNER 1974	⚲	6¼	22	10	6 2	18	FR	D	0 tpsl 2 cl grvl 20 lmst 22 *22
5451	" 875	XIV	2	R. HULBERT	K. HART 1973	⚲	6¼	36	20	7 2	36	FR	D	0 cl stns 18 lmst 36 *36
2169	" 925	XIV	3	R. VAN SCHARK	J.F. HENDERSON 1964	✕	6¼	75	DRY					0 dug 23 lmst 75
2170	" 921	XIV	3	R. VAN SCHARK	J.F. HENDERSON 1964	⚲	6¼	54	14	2½ 2	52	FR	D S	0 tpsl 1 cl stns 20 lmst 54 *52
2171	" 925	XIV	4	C. THOMAS	BALDWIN 1958	⚲	6	56	20	6.6 1	40	FR	D S	0 dug 24 hpn 52 lmst 56 *56

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5699	MARIPOSA TWP. 928	XIV	4	G. LONG	FAULKNER 1974	●	6¼	60	25	2½ 3	50	FR	D	0 tpsl 2 cl grvl 20 lmst. 60 *58
5725	" 928	XIV	4	G. LONG	FAULKNER 1974	●	6¼	100	48	1 1	99	FR	D	0 predrilled 60 lmst 100
2172	" 950	XIV	5	T. CROGGS	BALDWIN 1952	●	6¼	35	15	¼ -		FR	S	0 dug 15 cl 30 bldr 35 grvl 35+ * 16
2173	" 927	XIV	6	I. LICKLAER	BALDWIN 1967	●	10	74	27	1½ 2	70	FR	D	0 dug 28 lmst 74 *70
3571	" 940	XIV	6	W. APPEL	BALDWIN 1968	⊘	6¼.	107	25	½	–	SA	AB	0 cl hpn 18 lmst 107 *98
3572	" 935	XIV	6	W. APPEL	BALDWIN 1969	⊘	6¼	85	15	1/12	–	SA	AB	0 cl hpn 6 lmst 85 *80
3573	" 950	XIV	6	W. APPEL	BALDWIN 1968	●	6¼	35	14½	35 1	16	FR	D	0 cl hpn 13 lmst 35 *32
2174	" 950	XIV	8	G. OWENS	BALDWIN 1958	●	7	69	25	½ 1	69	FR	D S	0 cl stns 12 lmst 69 *40
2175	" 950	XIV	8	G. OWENS	BALDWIN 1958	●	7	128	30	½ 1	128	FR	D S	0 cl stns 15 lmst 128 *60
2176	" 942	XIV	8	W. THOMAS	BALDWIN 1958	●	7	50	24	3 1	50	FR	D S	0 dug 26 lmst 50 *45
2177	" 957	XIV	8	G. OWENS	J. F. HENDERSON 1966	✱	6¼	60	DRY					0 tpsl 2 cl stns 12 clsh 14 lmst 60
2178	" 949	XIV	8	H. IMRIE	BALDWIN 1958	●	4½	61	10	½ 1	61	FR	D S	0 dug 13 drilled 33 lmst 61 *13

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2179	MARIPOSA TWP 947	XIV	8	H. IMRIE	ALLARD BROS. 1961	⚲	2	42	18	1 1	–	Fr	D S	O cl & grvl 17 lmst 42 *40
2180	" 948	XIV	8	H. IMRIE	BALDWIN 1958	⚲	6½	72	20			Fr	D S	1 cl bldr 13 sh 20 lmst 72 * 50-72
2181	" 950	XIV	8	H. IMRIE	J.F. HENDERSON 1964	⚲	6¼	39	18	2 36	23	Fr	D S	O tpsl 2 cl & sh 16 lmst 39 *36
2182	" 949	XIV	8	H. IMRIE	J.F. HENDERSON 1964	✗	6¼	80	DRY					O cl 10 lmst 80
4680	" 950	XIV	8	B. NEILL	J.F. HENDERSON 1971	⚲	6	47	14	4½ 6	40	Su	S	O lm 2 cl & stns 14 lmst 47 *40
2193	" 900	XV	1	A. CONNING	J.F. HENDERSON 1961	⚲	6¼	35	10	2 5	25	Fr	D S	O tpsl 2 cl 14 cl & stns 26 sh 35 *35
2194	" 903	XV	2	J. DANCEY	J.F. HENDERSON 1965	⚲	6¼	67	35	2 7	60	Fr	D S	O stny cl 14 cl 60 lmst 67 *62
2195	" 925	XV	5	H. BUDD	J.F. HENDERSON 1963	⚲	6¼	37	10	3 18	20	Fr	D S	O tpsl 2 cl & crs snd 14 cl & stns 28 sh & lmst 37 *30
5709	" 925	XV	7	F. TREBELCO	KAWARTHA 1974	⚲	6¼	20	8	3 12	16	Fr	D	O cl stns 12 lmst sh 20 *18
2196	" 950	XV	9	H. DIXON	ALLARD BROS. 1961	⚲	2	36	18	2 ½	30	Fr	D S	O cl & bldrs 8 lmst 36 *35
2197	" 950	XV	9	H. DIXON	J.F. HENDERSON 1966	⚲	6¼	50	20	1 ½	48	Fr	D S	O tpsl 2 cl & sh 8 lmst 50 *30
4681	" 945	XV	9	H. DIXON	J.F. HENDERSON 1971	⚲	6	36	16	4½ 10	30	FR	D	O lm 2 cl & stns 7 lmst 36 *36

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2198	MARIPOSA TWP. 953	XV	10	UNITED CO-OP OF ONTARIO	J.F. HENDERSON 1965	●	6 1/4	58	25	10 4	50	Su	D	0 tpsl 2 cl 12 lmst 58 *58
4581	" 940	XV	10	K. DUKELOW	K. HART 1971	●	6 1/4	45	26	20 2	32	Fr	S	0 cl, bldr, stns 24 lmst 45 *37

MOE 0488 6/76

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536	ELDON TWP. 900	I	1	H. WACKERNAGEL	G. HART & SONS 1964	⚲	6¼	55	30	5		55	Fr	D S	O dug 30 lmst. 55 *32
537	" 872	I	3	R. VEALE	BALDWIN 1958	✱	7	45	DRY						O cl & stns 7 lmst 45
538	" 875	I	3	R. VEALE	J.F. HENDERSON 1961	✱	6¼	44	DRY						O tpsl 2 cl 8 sh 16 lmst. 44
539	" 875	I	3	R. VEALE	J.F. HENDERSON 1961	✱	6¼	40	DRY						O tpsl 2 cl 6 sh 14 lmst. 40
540	" 878	I	4	F. SWEET	J.F. HENDERSON 1965	⚲	6¼.	55	13	4		50	Fr	D S	O dug 15 lmst 55 *50
3553	" 875	II	3	W. KEELER	J.F. HENDERSON 1968	⚲	6¼	91	30	1	1½	90	Fr	D S	O dug 13 rk 91 *91
542	" 900	II	5	W. NEWMAN	BALDWIN 1952	●	6½	35	10	1	1	-	Fr	D	O cl 14 snd 15 cl snd grvl 21 crs grvl 35 *21
543	" 889	II	5	NEWMAN	BALDWIN 1952	⚲	6¼	42	18	½	1		Fr	D	O dug 23 sh & lmst 27 lmst 47 *40
544	" 896	II	5	A. CAMPBELL	ALLARD BROS. 1961	⚲	2	25	12	4	2	18	Fr	D	O cl & bldr 11 lmst 25 *25
545	" 886	II	5	LORNEVILLE PUBLIC SCHOOL	WILSON'S WELL DRILLING	●	36	16	9	-		-	Fr	School	O tpsl 1 cl 7 cl 9 crs grvl & bldr 16 *9
546	" 896	II	5	A. NEWMAN	BALDWIN 1966	●	6¼	20	13	6	1	16	Fr	D	O cl & hpn 18 grvl 20 *18
547	" 896	II	5	M. COOK	BALDWIN 1966	●	6¼	32½	10	8	1	24	Fr	D	O dug 14 cl, hpn 30 grvl 32½ *30

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Table Summary of Water Well Records

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Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm) (hrs)	Pumping Level (feet)	Quality	Use	Remarks, Log etc
548	ELDON TWP. 893	II	5	C. KNETT	BALDWIN 1966	●	6¼	52½	18^{1}	7	40	FR	D	O dug 17 cl, hpn 50 grvl 52½ *50
5645	" 880	II	5	R. COLLINS	K. HART 1974	♀	6¼	34	4^{2}	7^{2}	30	FR	D	O lm 2 cl 22 lmst 34 *34
5966	" 925	III	1	M. GORDON	K. HART 1974	♀	6¼	50	18	24^{2}	40	FR	D S	O. lm 2 cl & stns 8 lmst 50 *35
565	" 921	III	3	D. H. O.	BALDWIN 1963	♀̸	6¼	58	10	10	22½	SA	AB	O cl hpn 10 lmst 58 *56
567	" 898	III	4	D. H. O.	BALDWIN 1963	✱	6¼.	250	DRY					O tpsl 2 hpn 17 hpn 23 lmst 250
4830	" 875	III	5	B. MACALPINE	CLOSS WELL DIGGING 1971	●	30	38½	5	$10^{1½}$	38	FR	S	O cl 10 cl & grvl 25 cl 30 grvl 35 cl 38½ *15
586	" 955	IV	1	G. GRAHAM	FAULKNER 1964	♀	6¼	85	40	$⅙^{1}$	85	FR	D S	O tpsl 1 cl 14 cl & stns 26 lmst 85 *40
587	" 955	IV	1	G. GRAHAM	FAULKNER 1964	♀	6¼	108	40	$⅙^{1}$	108	FR	D S	O tpsl 1 cl 20 cl & stns 26 sh 31 lmst 108 *35
5963	" 940	IV	1	K. BUKELOW	K. HART 1974	♀	6¼	65	10	1^{2}	65	FR	D	O lm 2 cl & stns 10 lmst 65 *18
3752	" 940	IV	1	S. ALGER	J. F. HENDERSON 1969	♀	6¼	25	7	9^{2}	11	FR	D	O tpsl 2 cl & stns & sh 11 lmst 25 *23
588	" 939	IV	2	A. BENSON	BALDWIN 1949	♀	4⅞	34	10	1^{1}	–	FR	D S	O cl & grvl 15 lmst 34 *32
3555	" 950	IV	2	S. SUMMERBELL	J. F. HENDERSON 1968	✱	6	74	DRY					O tpsl, grvl 20 lmst 74

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Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm) (hrs)	Pumping Level (feet)	Quality	Use	Remarks. Log etc	
3556	ELDON TWP 950	IV	2	E. SUMMERBELL	J.F. HENDERSON 1968	⊗	6	50	DRY					0 tpsl, grvl 20 lmst 50	
589	" 950	IV	3	C. LILLICO	ALLARD BROS 1961	●	2	71	18	2 8	25	FR	D S	0 cl & bldr 35 lmst 71	*53
590	" 949	IV	3	LILLICO BROS	J.F. HENDERSON 1964	●	6¼	35	20	15 1	22	FR	D S	0 pit 5 cl 33 lmst 35	*34
3513	" 950	IV	3	L. THOMAS	J.F. HENDERSON 1968	●	6¼	32	15	8 2	25	FR	D	0 tpsl 2 cl stns 12 cl, sh 16 lmst 32	*30
597	" 955	V	1	H. COOLIDGE	BALDWIN 1964	●	6¼.	52	30	½ 1	47	F gas at 38'	D	0 cl hpn 20 sh lmst 24 lmst 52	*47-50
598	" 954	V	1	G. KELSEY	FAULKNER 1965	●	6¼	105	30	½ 3	100	FR	D S	0 tpsl 1 cl & stns 10 cl hpn 50 grvl, cl, snd 60 lmst 105	*50-70
599	" 952	V	2	H. COOLIDGE	BALDWIN 1952	●	6	35	15	5/6 1	—	FR	D	0 cl 13 lmst 35	*33
600	" 949	V	2	G. COOLIDGE	BALDWIN 1957	●	6	60	24	2 1	55	FR	D	0 cl 19 lmst 60	*55
5666	" 955	V	5	R. POLOZ	K. HART 1974	●	6¼	50	6	5 2	50	FR	D	0 cl & stns 3 sh 10 lmst 50	*38
5667	" 955	V	5	W. CHAPMAN	K. HART 1974	●	6¼	57	20	4 2	55	FR	D	0 lm 2 cl & stns 12 lmst 57	*57

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Table Summary of Water Well Records

Date

Prepared by

Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm)	(hrs)	Pumping Level (feet)	Quality	Use	Remarks Log etc	
3369	VILLAGE OF WOODVILLE 931			M. AUSTIN	BALDWIN 1950	📍	6	27	10	1/20			Fr	D	O cl & pbbl 9 lmst 27	*24
3370	" 932			S. MERRIAM	BALDWIN 1952	📍	6 1/4	43	29	1/2	1		Fr	D	O cl bldr 28 lmst 43	*41
3371	" 912			J. A. CAMPBELL	HART 1953	📍	5 5/8	22	12	3/4	1		FR	D	O cl & stns 7 lmst 22	*17
3372	" 931			R. HAWKINS	HART 1953	📍	5	23	14	1 1/2	1		Fr	D	O cl & stns 10 lmst 23	*20
3373	" 931			G. CAMPBELL	HART 1953	📍	5	37	26	1/2	1		Fr	D	O predrilled 18 lmst 37	*32
3374	" 951			J. CAMERON	HART 1955	📍	5	24	9	1/2	2	15	Fr	D	2 cl & stns 14 lmst 24	*24
3375	" 952			L. COOLIDGE	HART 1955	📍	5	67	30	1/12	1		Fr	D	O cl & stns 30 lmst 67	*35
3376	" 921			O. E. THORPE	HART 1955	📍	5	44	14	2/3	1		Fr	D	O cl & stns 15 lmst 44	*40
3377	" 929			McPHERSON	BALDWIN 1956	📍	5 5/8	45	10	1 1/2	1	12	Fr	D	O cl 32 lmst 45	*45
3378	" 930			W. J. McPHERSON	BALDWIN 1957	📍	5 5/8	43	20	1 1/2	1		Fr	D	O cl 26 lmst 43	*40
3379	" 930			D. SPENCE	BALDWIN 1956	📍	5 5/8	33	20	1 1/2	1		Fr	D	O cl 16 lmst 33	*30
3380	" 942			W. CAMERON	BALDWIN 1958	📍	6	44	10	3	1	35	Fr	D	O cl & bldr 20 lmst 44	*40

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Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm) (hrs)	Pumping Level (feet)	Quality	Use	Remarks, Log etc
3381	VILLAGE OF WOODVILLE 948			UNITED CHURCH	BALDWIN 1958	●	6	34	18	3½ 1	34	FR	D	O cl & bldr 20 lmst 34 *30
3382	" 932			D. BROWNLEE	BALDWIN 1958	●	6	28	10	3 1	25	FR	D	O cl 12 lmst 28 *26
3383	" 930			R. BURTON	BALDWIN 1958	●	6	168	15	½ 1	168	Su FR?	D	O tpsl & bldr 10 lmst 168 *168
3384	" 942			F. OWENS	BALDWIN 1958	●	7	63	31	3 1	63	FR	D	O cl & bldr 29 lmst 63 *55
3385	" 931			O. LANE	HART 1958	●	7	36	7	½ 2	30	FR	D	O cl & stns 12 lmst 36 *30
3386	" 936			B. LAMB	BALDWIN 1958	●	7	50	20	2 1	50	FR	D	O cl & stns 11 lmst 50 *40
3387	" 928			M.P. AUSTIN	BALDWIN 1959	●	6½	29	10	10 1	29	FR	D	1 cl & stns 8 lmst 29 *29
3388	" 952			DR. J. ANDERSON	BALDWIN 1959	●	6½	80	25	5 1	80	FR	D	O cl & bldr 40 lmst 80 *70
3389	" 942			E. THOMPSON	BALDWIN 1960	●	6¼	45¾	30	1½ 1	30	FR	D	O dug 24½ lmst 45¾ *40
3390	" 932			O. LAMB	BALDWIN 1960	●	6¼	115	—	—	—	—	D	O cl 5 hpn 17 lmst 115
3391	" 927			BELL TELEPHONE	K. HART 1961	✕	6¼	115	DRY					O cl & fill 16 lmst 115
3392	" 927			BELL TELEPHONE	K. HART 1961	●	6¼	50	10	1 2	48	FR	D	O cl 9 lmst 50 *48

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Table Summary of Water Well Records

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Prepared by

Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm) (hrs)	Pumping Level (feet)	Quality	Use	Remarks: Log etc
3393	VILLAGE OF WOODVILLE 929			MRS. J. KING	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	29	11	6^{1}	19	FR	D	0 tpsl 2 cl 8 sh 10 lmst 29 *28
3394	" 939			MRS.E. KING	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	24	9	10^{1}	11	FR	D	0 tpsl 2 cl 10 sh 15 lmst 24 *23
3395	" 938			U. FISHER	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	41	19	3^{1}	24	FR	D	0 tpsl 2 cl 12 lmst 41 *39
3396	" 931			F. McEACHERN	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	38	15	3^{1}	27	FR	D	0 tpsl 2 cl 15 sh 16 lmst 38 *37
3397	" 942			S. NEWMAN	BALDWIN 1961	●	$6\frac{1}{4}$	$40\frac{1}{4}$	20	3^{1}	35	FR	D	0 cl 3 hpn 8 lmst $40\frac{1}{4}$ *20 *35
3398	" 940			CANADIAN LEGION	BALDWIN 1961	●	$6\frac{1}{4}$	$34\frac{3}{4}$	15	4^{1}	30	FR	D	0 cl 2 hpn 15 lmst $34\frac{3}{4}$ *30
3400	" 930			KNOX PRES. CHURCH	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	60	20	$1\frac{1}{2}^{2}$	56	FR	D	0 cl 16 sh 24 lmst 60 *55
3401	" 929			A. JEWELL	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	41	20	$1\frac{1}{2}^{2}$	37	FR	D	0 dug 24 fngrvl 31 sh 41 *41
3402	" 942			J. MONTAGUE	J.F. HENDERSON 1961	●	$6\frac{1}{4}$	45	23	2^{2}	40	FR	D	0 tpsl 2 cl 16 sh 22 lmst 45 *45
3403	" 942			K. HANDCOCK	J.F. HENDERSON 1963	●	8	47	20	$2\frac{1}{2}^{2}$	42	FR	D	0 tpsl 2 cl :stns 12 cl :sh 20 lmst 47 *40
3405	" 942			H. CAMERON	J.F. HENDERSON 1963	●	8	40	14	1^{3}	34	FR	D	0 dug 6 lmst 40 *20
3406	" 927			G. ENGLISH	J.F. HENDERSON 1964	●	$6\frac{1}{4}$	54	9	1^{3}	50	FR	D	0 tpsl 2 cl 19 lmst 54 *51

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Table Summary of Water Well Records

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Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm)	(hrs)	Pumping Level (feet)	Quality	Use	Remarks, Log etc
3407	VILLAGE OF WOODVILLE 938			MRS. J. B. CRAMER	BALDWIN 1964	●	6 1/4	80	22	3/4	1	70	FR	D	O dug 13 hpn & stns 26 brk lmst 28 lmst 80 *72
3408	" 930			BANK OF COMMERCE	J.F. HENDERSON 1964	●	6 1/4	58	18	2	4	28	FR	D	O dug 18 lmst 58 *58
3409	" 926			H. WHITFIED	J.F. HENDERSON 1965	●	6 1/4	17	5	3	3	15	FR	D	O tpsl 2 stny cl 12 lmst 17 *17
3410	" 921			M. McKAQUE	FAULKNER 1964	●	6 1/4	64	40	1/2	1	63	FR	D	O cl & stns 12 sh lmst 15 lmst 64 *48
3411	" 933			H. CAMERON	J.F. HENDERSON 1965	⊗	6 1/4	50	DRY					AB	O stny cl 10 lmst 50
3412	" 933			H. CAMERON	J.F. HENDERSON 1965	⊗	6 1/4	80	DRY					AB	O stny cl 12 lmst 80
3413	" 934			H. CAMERON	J.F. HENDERSON 1965	●	6 1/4	50	10	1/2	1	50	FR	D	O stny cl 12 lmst 50 *35
3414	" 925			G. DAY	J.F. HENDERSON 1965	●	6 1/4	36	14	15	2	25	FR	D	O dug 18 lmst 36 *32
3415	" 942			L. ARCHIBALD	J.F. HENDERSON 1965	●	6 1/4	76	8	6	2	65	FR	D	O dug 20 stny cl 48 lmst 76 *48-65
3416	" 951			A. BELL	J.F. HENDERSON 1965	●	6 1/4	68	21	5	2½	60	FR	D	O cl lm 1 sndy cl 8 cl 46 lmst 68 *66
3417	" 939			DR. J.B. CRAMER	BALDWIN 1965	●	10 1/4	55½	25	1	1	40	FR	D	O pit 5 cl hpn 10 lmst 55½ *40
3418	" 879			MRS. M. CHROUCHMAN	J.F. HENDERSON 1966	●	6 1/4	39	12	6	2	29	FR	D	O tpsl 2 cl, stns, sh 25 lmst 39 *35

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Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm) (hrs)	Pumping Level (feet)	Quality	Use	Remarks, Log etc
3419	VILLAGE OF WOODVILLE 926			S. MURRAY	BALDWIN 1966	●	6¼	26½	18½	$15^{1/2}$	21½	FR	D	O hpn 11 lmst 26½ *26
3420	" 955			B. PETHICK	J. F. HENDERSON 1967	●	6¼	95	35	3^{4}	90	FR	D	O tpsl 1 cl & grvl 44 lmst 95 *90
3421	" 942			MRS. A. THORNBURY	J. F. HENDERSON 1967	●	6¼	101	60	$\frac{1}{4}^{4}$	101	FR	D	O tpsl 2 cl 12 lmst 101 *90
3422	" 931			P McCARTHY	BALDWIN 1967	●	6¼	35	15	$2\frac{1}{2}^{1/2}$	30	FR	D	O hpn 14 lmst 35 *18
3567	" 930			E. BARBER	J. F. HENDERSON 1968	●	6⅝.	31	15	5^{2}	25	FR	D	O tpsl 14 lmst 31 *31
3568	" 950			G. ENGLISH	J. F. HENDERSON 1968	●	6¼	118	75	10^{1}	85	FR	D	O tpsl 6 cl 48 lmst 118 *118
3570	" 925			S. KELSEY	BALDWIN 1968	●	6¼	19½	10	10^{2}	13	FR	D	O cl hpn 14½ sh brk lmst 17½ cl 18½ lmst 19½ *14
3512	" 950			J. MONTAQUE	J. F. HENDERSON 1968	●	6¼	69	35	4^{2}	60	FR	D	O tpsl 2 cl & stns 40 cl grvl 43 lmst 69 *67
3786	" 925			O. W. R. C. TH-3-69	K. HART 1969	⊘	8	41½	4	$21^{1/4}$	35	FR	M AB	O cl stns 12 sh 14 lmst 41½ * 14 18
3787	" 935			O. W. R. C. TH-1-69	K. HART 1969	○	8	42	2	40^{8}	11	FR SA	M	O snd 12 sh 15 lmst 42 *20 *30SA
3788	" 935			O. W. R. C. TH-2-69	K. HART 1969	⊘	8	29	8	28^{1}	26	FR SA	M AB	O fill 4 cl stns 10 snd 15 sh 16 lmst 29 *22 *29SA
3789	" 925			O W R C TH-6-69	K. HART 1969	○	8	30	7	75^{68}	12	FR	M	O cl stns 12 lmst 30 *20 *28

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Ontario

Table Summary of Water Well Records

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Well No	Location and Elevation	con	lot	Owner	Driller year	Well Type	Well Diameter (inches)	Depth (feet)	Static Level (feet)	Pumping Test (gpm)(hrs)	Pumping Level (feet)	Quality	Use	Remarks Log etc
3790	VILLAGE OF WOODVILLE 925			O.W.R.C. TH-5-69	K. HART 1969	○	8	38	8	40 24	15	FR	M	O cl stns 8 grvl 19 lmst 38 *19 30 39
3791	" 925			O.W.R.C TH-4-69	K. HART 1969	⊘	8	39	8	21 1/4	30	FR	M AB	O cl stns 8 grvl 12½ lmst 39 *15 30
3892	" 925			J McINTYRE	J.F. HENDERSON 1969	●	6 1/4	93	35	6 2	82	FR	D	O tpsl 2 cl & stns 14 cl sh 22 lmst 93 *90
4711	" 940			H. WEBSTER	BALDWIN 1972	⊗	6 1/4	60	DRY				AB	O cl & bldr 10 sh lmst 19 lmst 60
4712	" 940			H. WEBSTER	BALDWIN 1972	⊗	6 1/4.	240	DRY				AB	O cl & bldr 10 sh lmst 19 lmst 240
4713	" 935			R. JONES	BALDWIN 1972	●	6 1/4	60	15	2 1	40	FR	D	O cl & bldr 15 lmst 60 *30

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Table 2 Summary of Water Analyses

Prepared by J.K. Yee

										Chemical Constituents in parts per million (ppm)											
Source and Number	Location	Date Sampled	pH	Colour Hazen Units	Turbidity Jackson Units	Specific Conductance mmhos at 25°C	Total Dissolved Solids (ppm)	Total Hardness as $CaCO_3$ (ppm)	Alkalinity as $CaCO_3$ (ppm)	Chloride (Cl)	Sulphate (SO_4)	Iron (Fe)	Calcium (Ca)	Magnesium (Mg)	Sodium (Na)	Potassium (K)	Free Amonia	Total Kjeldahl	Nitrite	Nitrate		Remarks
Bryan Residence (Town supply)	Woodville Area	Feb.7/ 77	7.3			650	372	348	268	21	33	.01	123	10	8	29	.1	.1	.02	97		
Jones Well 3387	"	"	7.1			1140	686	532	382	88	63	.03	162	31	41	120	.1	.2	.03	17.0		
Hembruff Well 3377	"	"	7.2			1000	636	472	303	106	43	.06	162	16	30	4.9	.1	.1	.01	12.0		
Cameron Residence (Town supply)	"	"	7.4			670	392	357	278	22	33	.01	126	10	8	3.1	.1	.1	.01	99		
White Creek at Hwy. 46	"	"	7.9			610	386	330	268	19	27	1.58	115	10	6	2.4	.1	.7	.03	68		
Fiske Well	"	"	7.4			1100	640	451	406	120	34	.09	157	14	72	20	.1	.2	.01	.4		Rock 18' deep
Lane Well 3385	"	"	7.4			810	456	381	313	64	56	.69	88	39	36	4.7	.2	.3	.01	.1		
White Well	"	"	7.4			850	522	7	263	42	92	.03	3	.1	205	1.3	.1	.2	.02	10.0		
Baker Well	"	"	7.7			480	266	264	233	9	34	.86	52	8	7	2.1	.1	.1	.01	.1		

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CC&S MICROGRAPH

GC -56

TEN YEARS BY MONTHS X 100 DIVISIONS

MADE IN CANADA

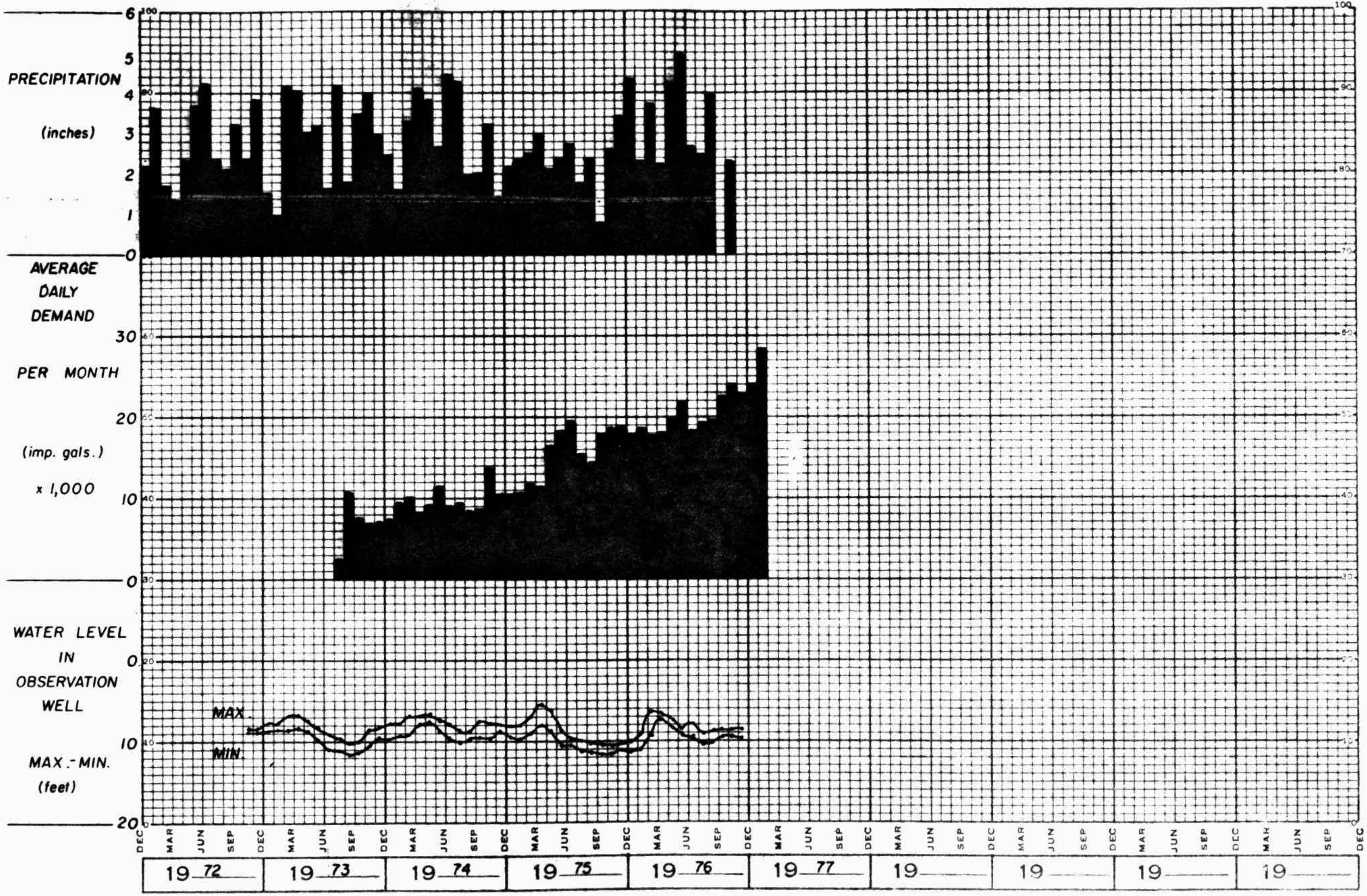
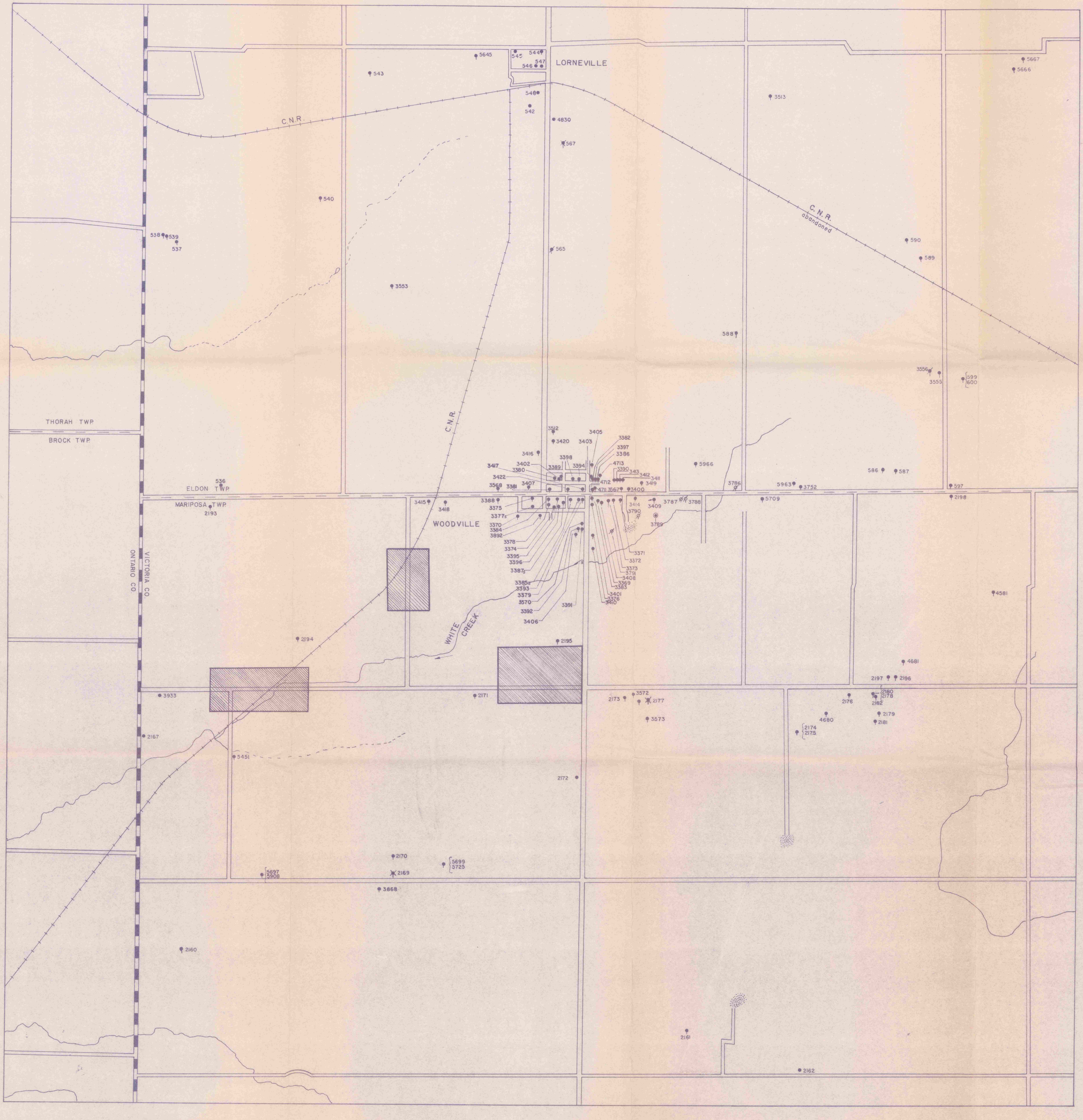


FIGURE 2



VILLAGE OF WOODVILLE

WATER WELL LOCATIONS AND FAVOURABLE TEST DRILLING AREAS

NORTH

SCALE
1 inch = 1,000 feet

LEGEND

3423	*Well number*
●	*Drilled well in overburden*
●	*Drilled well in bedrock*
⌀	*Testwell (abandoned)*
⌀	*Drilled well in bedrock, (abandoned due to poor quality)*
✕	*Drilled well in bedrock, (abandoned, dry hole)*
← ●	*Flowing drilled well in bedrock*
3423 s	*Sampled well or location*
▨	*Favourable test drilling areas*
◉	*Drilled municipal well in bedrock*

FIGURE NO. 1 AUGUST 1977 J.K.Y.